Integrated Noise Model (INM) Noise Contour Comparison: Version 7.0 vs. 6.2a

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1. Introduction

Version 7.0 of the Integrated Noise Model (INM) was released on April 30, 2007. Relative to the INM 6.x series (INM 6.0, 6.0a, 6.0b, 6.0c, 6.1, 6.2 and 6.2a), version 7.0 is more sophisticated and comprehensive, as well as compliant with recently published global standards such as ECAC Doc 29¹.

Similar to previous major releases, the new methodologies used in version 7.0 results in different noise predictions, as compared with previous versions. Some of the new methodologies are expected to increase noise levels, while others may result in decreases. The degree of the changes depends on many factors such as fleet mix, runway configuration, terrain etc. Therefore, it is not realistic to examine just one individual airport and draw conclusions about INM7.0 noise contour change.

This report provides FAA regional officers and others involved with environmental projects a general sense of noise level changes expected by using version 7.0 based on multiple airport studies. Four airports were investigated using both versions 6.2a and 7.0. The four airports were selected to represent geographic diversity and different airport types, as represented by variations in operations, fleet mix and runway layouts. Through detailed review and analysis of noise results for different cases, the report helps the reader to understand the potential range of the noise level changes, some key elements that cause the changes, putting into context the potential change that may be expected at the airport of their particular interest.

The report is organized into four sections. Section 2 provides an overview of the new methodologies implemented in version 7.0, and focuses on several elements that could cause noise contour changes. Section 3 introduces the four airport modeling studies and describes the sensitivity study, including descriptions of the study parameters investigated. It also reviews INM outputs and typical results. Section 4 presents noise contour changes of the modeling studies, and associated discussion and analysis on the results. A summary at the end, Section 5, ties the results together and makes suggestions on how these conclusions should be used.

2. Overview of INM Version 7.0 Noise Modeling Methodology

INM has been the FAA's standard tool for airport noise assessments since 1978. INM is used domestically and throughout the world. Currently, the INM 6 and 7 series are used by over 1000 organizations in over 65 countries, with the user base increasing every year. About 200 version 7.0 boxes were shipped within three months of its release in April 2007. Table 1 shows percent by user of the first 200 users of INM7.0.

¹ European Civil Aviation Conference (ECAC) Doc 29 (3rd Edition) "Report on Standard Method of Computing Noise Contours around Civil Airports Volume 1: Applications Guide; Volume 2: Technical Guide" July 2005

Table 1. Percent by User of the First 200 Users of INM7.0 (May-August, 2007)

Type of User	Percent
Commercial	62%
FAA Regions	10%
Education	9%
Airliner	8%
Other government	6%
Other Users	5%

2.1 General Features of Version 7.0

The release of version 7.0 represents a significant step forward in the capability to model potential noise impacts due to aviation sources.

Version 7.0 includes the following new operational and computational features:

- Improved helicopter noise modeling capabilities based on the Heliport Noise Model (HNM) Version 2.2 which includes;
 - Helicopter-specific noise-power-distance (NPD) data and directivity implementation; and
 - o Expanded helicopter operational modeling functionality.
- Compliance with ECAC Doc 29, which includes:
 - o New SAE-AIR-5662 lateral attenuation adjustment algorithms;
 - Updated thrust reverser implementation;
 - o Bank angle implementation;
 - o Updated flight path segmentation; and
 - o Additional procedural profile step types.

INM 7.0 also includes new software features. The most significant is the Scenario-Case Format, which allows for further categorization of input data within an INM study; and allows for annualization, where a user may adjust noise contributions of individual Cases in a Scenario by a scale factor and an annualization percentage without re-running that Scenario. The new software features improve the software usability and improve the modeling and running efficiency. Table 2 summarizes the new features in INM7.0 in comparison to the previous versions.

Table 2. INM 7 Features in Comparison to Previous Versions

Release Date I. Modeling Advanced Modeling helicopters, tracks and profiles (integrated Heliport Noise Model [HNM] Version 2.2 capabilities) Modeling helicopters, tracks and profiles (partial implementation of HNM helicopters as fixed-wing aircraft) Commercial, military and user-defined aircraft, tracks and profiles Compliance with SAE-AIR-1845 (1986) Compliance with ECAC Doc 29 (3 rd Edition, 2005) - Bank angle - New flight procedure step types - Updated thrust reverser noise implementation Thrust reverser noise Run-up noise 2. Noise Computations Distributed and Multi-threaded processing Single-computer processing Scenario Annualization Lateral attenuation - Based on SAE-AIR-5662 (2006 - in replacement of SAE-AIR -1751) - Based on enhanced SAE-AIR-1751 (1981, and differentiating between engine-mounting configurations) - Based on SAE-AIR-1751 (1981)	X X X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	X X X X X
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- Bank angle - New flight procedure step types - Updated thrust reverser noise implementation Thrust reverser noise Run-up noise 2. Noise Computations Distributed and Multi-threaded processing Single-computer processing Scenario Annualization Lateral attenuation - Based on SAE-AIR-5662 (2006 - in replacement of SAE-AIR -1751) - Based on enhanced SAE-AIR-1751 (1981, and differentiating between engine-mounting configurations) - Based on SAE-AIR-1751 (1981)	X X X X X X X X X	X	X	X	X
- New flight procedure step types - Updated thrust reverser noise implementation Thrust reverser noise Run-up noise 2. Noise Computations Distributed and Multi-threaded processing Single-computer processing Scenario Annualization Lateral attenuation - Based on SAE-AIR-5662 (2006 - in replacement of SAE-AIR -1751) - Based on enhanced SAE-AIR-1751 (1981, and differentiating between engine-mounting configurations) - Based on SAE-AIR-1751 (1981)	X X X X X X X	X	X	X	X
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between engine-mounting configurations) - Based on SAE-AIR-1751 (1981)					
- Based on SAE-AIR-1751 (1981)		X	X	X	
					X
- Ability to turn off lateral attenuation for helicopters and propeller					
aircraft	X	X	X		
	X	X	X		
Ability to limit computations to locations within a user-defined					
geographic boundary	X	X	X		
3. Databases					
New aircraft noise and performance data	X	X	X	X	X
	X	X	X	X	X
	X	X	X		
	X	X	X	X	X
4. Format and Input/Output					
	X				
	X	X	X	X	X
	X				
Import DXF, Polyline TXT, Census 2000, and Radar Track CSV files	X	X	X	X	X
Expanded ability to process and import Census Tiger/Line data	X	X	X	X	
<u> </u>	X	X	X	X	X
	X	X	X		
Ability to export noise contours and other visual layers to ESRI	v			v	
Shapefiles	X	X	X	X	
Ability to export noise contours and other visual layers to MapInfo	v	v	v		
Data Interchange Format files	X	X	X		
5. Metrics					
A-weighted, C-weighted and tone-corrected Metrics	X	X	X	X	X
	X	X	X	X	X
Supplemental noise metrics: Time Audible (TAUD) and Change in Exposure (DDOSE)	X	X	X		
*	X	X	X		

[1] Helicopter Noise Modeling was first introduced in INM Version 6.0c.

2.2 One Specific INM Modeling Methodology – Lateral Attenuation Adjustment

The version 7.0 technical manual will be released at the end of 2007. It provides in depth descriptions of existing and new methodologies implemented in INM. This section provides an overview of the lateral attenuation adjustment, due to its potential impact to noise contours.

The difference in level between the sound directly under the aircraft's flight path and a location to the side of the aircraft at the time of closest approach is termed "lateral attenuation." The lateral attenuation adjustment takes into account a combination of three elements:

- engine installation effect (airplane shielding effect, function of engine type and depression angle φ)
- ground-to-ground attenuation (ground reflection effect, function of empirical parameter of lateral distance ℓ)
- air-to-ground attenuation (refraction effects, function of empirical parameter of elevation angle β)

Figure 1 displays the lateral attenuation geometry. Note that if the aircraft altitude is known, elevation angle β and lateral distance ℓ are dependent on each other. Similarly, when bank angle ϵ is known, depression angle φ is linearly related to elevation angle β .

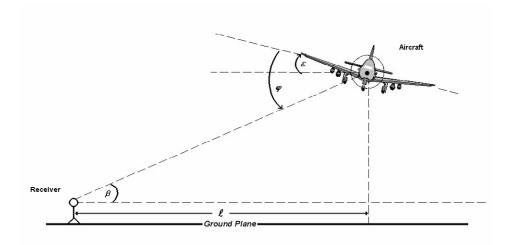


Figure 1. Illustration of bank angle ϵ , elevation angle β , depression angle ϕ , and lateral distance ℓ .²

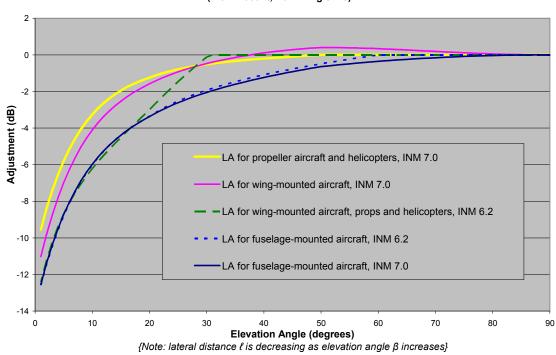
Figure 2 shows an example of the composite lateral attenuation adjustment for both versions 6.2a and 7.0 as a function of elevation angle. In this example the altitude is at 1,000 ft and bank angle is 0°. The slant distance decreases as elevation angle increases. Using different combinations of altitudes and bank angles will result in different magnitudes of lateral attenuation adjustments. A negative value means that the lateral attenuation adjustment is to be subtracted from the system noise equation. When all other variables are held constant, a smaller magnitude lateral attenuation adjustment results in higher noise levels and correspondingly larger noise contours.

In Figure 2 the dashed and dotted lines are version 6.2a results, representing adjustments corresponding to wing-mounted and fuselage-mounted engines on jet aircraft, respectively. In version 6.2a, the adjustment for props and helicopters were approximated by that of the wing-mounted engine aircraft. In contrast, version 7.0 has three separate lateral attenuation adjustment curves: one for jets with fuselage-mounted engines, with the curve similar to that of version 6.2a; one for jets with wing-mounted engines, with the curve above that of version 6.2a; and one for props and helicopters.

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² Source: SAE-AIR-5662, Method for Predicting Lateral Attenuation of Airplane Noise, 2006.

A few observations can be noted: (1) the separation of the lateral attenuation adjustments among different aircraft types in INM7.0 tends to be more significant at small elevation angles; (2) the change in lateral attenuation adjustment in INM7.0 is more pronounced for props than for jets.



Lateral Attenuation Comparison between INM 6.2/6.2a and INM 7.0 (Alt. = 1000 ft, Bank Angle = 0)

Figure 2. Composite Lateral Attenuation Adjustment

3. INM7.0 Noise Contour Comparison & Studies

Four airports were studied using both versions 6.2a and 7.0. The four airports were selected to represent geographic diversity and different airport types as well as variation in operations, fleet mix and runway layout.

Table 3 lists the fleet mix of the four airports in this study. The airports are referred to as "Western", "Eastern", "LgHub" and "LgGA", respectively. The several columns of fleet mix information are based on the study files available for this study. In the table, the columns represent the following for each study: percent of jets with wing-mounted engines [A], percent of jets with fuselage-mounted engines [B]; and percent of props [C] and percentage of helicopters [D].

		Percent of Operations							
		Α	В	С	D				
Airports	Study Files	Wing-Mounted Engine - Jet	Fuselage- Mounted Engines - Jet	Prop	Helo				
"Western"	2003	69	14	17	0				
"Eastern"	2003	64	9	27	0				
"LgHub"	2000	47	46	7	0				
"LgGA"	1996	25	6	67	2				

Table 3. Study Airports and Fleet Mix Information

3.1 INM Runs for Noise Contour Comparison

INM runs were conducted to evaluate the DNL and LAMAX metrics in both versions 6.2a and 7.0. Initially, baseline settings were established and the contours and contour areas comparing the two versions were documented for both DNL and LAMAX. Subsequently, the effects of five different INM settings were analyzed on a one-by-one. Three of the variables were chosen to reflect the major changes to the INM software between versions and are listed below:

- 1. terrain (segmentation, geometry);
- 2. lateral attenuation (SAE-AIR-5662 implementation in "All Soft Ground", turning off attenuation for props and helicopters in "No-Prop-Attenuation");
- 3. bank angle (aircraft geometry, aircraft performance, SAE-AIR-5662 implementation)

In addition, two variables that were not directly altered between the versions were chosen. These variables, temperature and headwind, effect aircraft performance and will illustrate the affect of aircraft performance given the above changes between versions.

The results from these studies were plotted as contours and compared. They were compared according to metric, INM version, and status of the variable under consideration, which resulted in the test matrix shown in Table 4. It should be noted that helicopters within the studies were modeled as user-defined fixed wing aircraft in both versions of the model. Though version 7.0 does incorporate HNM 2.2 capabilities, it was determined that the effects of this new capability in version 7.0 will be better explored by single event studies.

The baseline settings were

- Terrain = Off
- Lateral Attenuation = No Prop Attenuation
- Bank Angle = Off
- Temperature = 59° F
- Headwind = 8 Knots

The Terrain "Off" option assumes a flat surface. No line-of-sight (LOS) blockage is examined in this case.

The "No-Prop-Attenuation" option does not utilize the special lateral attenuation adjustment for props and helicopters, but still applies SAE-AIR-5662 adjustment to jets. In contrast, the "All-Soft-Ground" option applies the SAE-AIR-5662 adjustment to all aircraft types.

The Bank Angle "Off" option deactivates the bank angle methodologies implemented in version 7.0. In general, the effect of bank angle on or off varies from study to study depending on the curvature of the utilized ground tracks.

The temperature and headwind in the baseline case are the standard settings (59 degrees F and 8 knots) in INM. Variation is introduced in other study cases.

During each case study, constant settings were applied to

• Do Contours = On

 Recursive Grid (DNL Refinement = 6, Tolerance = 1; LAMAX Refinement = 4, Tolerance = 1)

Results are presented in tabular form. The DNL range, chosen with regulatory requirements in mind, is between 55 and 70 dB, while the LAMAX values range between 90 and 105 dB.

Table 4: Sensitivity Test Matrix

			Modeling S	ettings in INN			
Study Name	Config. #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
Baseline	C1	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	8 Knots
STUDY with Terrain	C2	6.2a/7.0	On	No Prop Attenuation	Off	59°F	8 Knots
STUDY with and without Terrain, 7.0 Release Only	СЗ	7.0 only	On/Off	No Prop Attenuation	Off	59°F	8 Knots
STUDY with Lateral Attenuation On (All Soft Ground)	C4	6.2a/7.0	Off	All Soft Ground	Off	59°F	8 Knots
STUDY with and without Lateral Attenuation, 7.0 Release Only	C5	7.0 only	Off	All Soft Ground / No- Prop-	Off	59°F	8 Knots
STUDY 6.2a Baseline vs. 7.0 Release with Bank Angle	C6	6.2a/7.0	Off	No Prop Attenuation	On	59°F	8 Knots
STUDY, 7.0 Release with and without Bank Angle	C7	7.0 only	Off	No Prop Attenuation	On/Off	59°F	8 Knots
STUDY at 100° F	C8	6.2a/7.0	Off	No Prop Attenuation	Off	100°F	8 Knots
7.0 Release at 59° F and 100° F	C9	7.0 only	Off	No Prop Attenuation	Off	100°F/59°F	8 Knots
STUDY at 32° F	C10	6.2a/7.0	Off	No Prop Attenuation	Off	32°F	8 Knots
7.0 Release at 59° F and 32° F	C11	7.0 only	Off	No Prop Attenuation	Off	32°F/59°F	8 Knots
STUDY with -8 Knot Headwind	C12	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	-8 Knots
7.0 Release with +8 Knot and -8 Knot Headwind	C13	7.0 only	Off	No Prop Attenuation	Off	59°F	-8/+8 Knots
STUDY with Zero Headwind	C14	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	0 Knots
7.0 Release with 8Kt and Zero Headwind	C15	7.0 only	Off	No Prop Attenuation	Off	59°F	8 / 0 Knots
STUDY All Variables On	C16	6.2a/7.0	On	All Soft Ground	On	59°F	8 Knots
Baseline vs. All Variables On, 7.0 Release	C17	7.0 only	On/Off	All Soft Ground / No- Prop- Attenuation	On/Off	59°F	8 Knots

In cases C16 and C17, the label "All Variables On" indicates that the three non-meteorological settings (Terrain, Bank Angle, and Lateral Attenuation All Soft Ground) were all activated in the studies.

3.2 **Preliminary Results and Examination**

Figure 3 shows a typical DNL noise contour from an airport, generated by versions 6.2a and 7.0, respectively.

Table 5 shows the DNL and LAMAX noise contour results, and relative difference in contour areas between the two versions.

Several observations can be made:

- 1. The DNL noise contours are similar in shape for the two versions of INM.
- 2. In this case, version 7.0 increased the noise contour area. In this case setting, for DNL, the noise contour change was less than 8%, with the max increases around DNL65 dB and DNL60 dB range.
- 3. As shown in Table 5, the LAMAX contour area change did not follow the DNL contour change. This was likely caused by unique fleet situation. That is, the LAMAX at each grid point did not alter between version 6.2a and version 7.0.

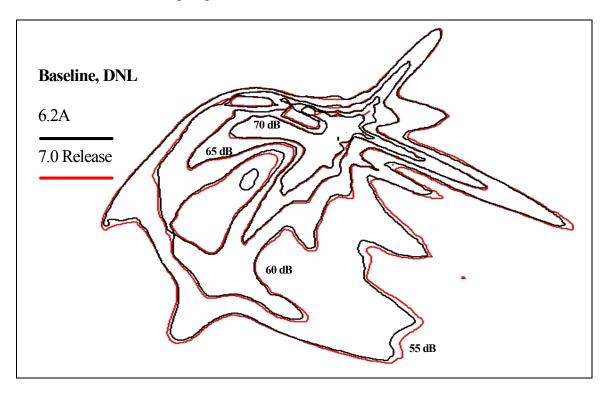


Figure 3. Baseline (C1) DNL Contour of Airport "Eastern"

Table 5. The Associated Contour Areas for DNL and LAMAX

8 1

7.2

53.045

18.643

7.746

	0.2/	/_I\ClCa3C	
INM Version:	(LAMAX)	(LAMAX)	DELTA (7 - 6.2A)
LAMAX LEVEL	SQ.MI	SQ.MI	% SQ. MI
90	155.158	158.636	2.2
95	80.239	82.593	2.9
100	28.678	29.864	4.1
105	14.334	14.876	3.8

7 Release

The study presented above is one example of the data created for this report. The results for all the runs were condensed to gain better insight into the data. The contour differences are shown in a side-by-side for all four airports in the next section.

4. Results and Discussion

49.073

17.396

60

65

The following section contains results and observations for each contour comparison conducted in this sensitivity study. For each comparison (as described in Section 3.1), the INM Study parameters are presented first, followed by tables showing the percent change in contour area between versions 6.2a and 7.0, for each metric investigated.

Positive values indicate an increase in percent contour area in version 7.0, as compared to version 6.2a. Negative results are displayed in parentheses (e.g., -1.63% is (1.63) in Table 6). Observations and discussion pertaining to these results are presented at the end of each subsection.

4.1 Baseline Contour Area Data (C1)

Table 6. Baseline Contour Area Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
Baseline	C1	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	8 Knots

DNL	% Area Change INM7.0 vs INM6.2a						
LEVEL	Western	Eastern	LgHub	LgGA			
55	5.65	5.71	3.32	10.76			
60	6.04	8.09	3.07	9.38			
65	5.74	7.17	3.16	9.34			
70	3.21	4.11	1.38	11.03			

LAMAX	% Area Change INM7.0 vs INM6.2a						
LEVEL	Western	Eastern	LgHub	LgGA			
90	(0.19)	2.24	(0.88)	(1.63)			
95	(3.45)	2.93	(2.89)	(0.82)			
100	(3.64)	4.14	(3.01)	(2.89)			
105	(4.45)	3.78	(5.33)	(1.67)			

Observations and Discussion:

As shown in Table 6, the 65 dB DNL contour areas increased less than 10% for the four airports studied.

The changes can likely be attributed to two factors: segmentation and lateral attenuation. Segmentation changes can effect overall contour shape. The change in lateral attenuation implementation leads to changes to the corresponding noise level adjustments, as discussed in Section 2.1. While the lateral attenuation adjustments may vary according to study geometry, aircraft position relative to the receiver, and aircraft type, many cases result in lateral attenuation adjustments that are smaller in version 7.0 than 6.2a (Figure 2), which may result in an increase in noise contour area. This is especially significant for jets with wing-mounted engines, since no lateral attenuation adjustment is applied to props and helicopter for this baseline setting.

In general, the DNL noise contour increase varies from one airport to another, and the magnitude of the change in the DNL contour seems to correlate with the percentage of jets with wing-mounted engines in the fleet. For example, the "LgHub" has the smallest DNL contour change (3.2% for 65 dB DNL) and its jets with wing-mounted engines are only 47% of the total fleet. The "Western" and "Eastern" airports show higher 65 dB DNL contour changes, but the percentage of jets with wing-mounted engines in their fleets is also higher. At first look, the "LgGA" is an apparent exception to this observation. It has largest the DNL contour change of the four airports, and yet shows the least percentage of the jets with wing-mounted engines in the total fleet. Examination of Table 2 reveals that the fleet of "LgGA" is dominated by props, rather than by jets, as seen at the three other airports. The percentage of jets with wing-mounted engines in the jet fleet of "LgGA" is actually on par with that of "Eastern" and "Western". A separate study excluding the props indicated that the jets, although out-numbered by props in "LgGA", had significant noise contribution.

The percent of jets with wing-mounted engines in the fleet can be used as an indicator of the DNL contour change, but other factors play a role as well, such as relative noise contribution of different types of aircraft to the noise contour.

LAMAX contour area changes show quite a different picture from DNL (See Table 6). Except for "Eastern", all airports actually show a decrease in the LAMAX contour size in version 7.0. While DNL contour area changes may be related to updates that affect the entire fleet, LAMAX contours are typically dominated by single aircraft. Such is the case for the "Eastern" airport, which is dominated by a prominent jet with wing mounted engines, resulting in consistent trend with DNL due to the lateral attenuation effect discussed previously. The other three airport studies, on the other hand, happen to be dominated by a prominent jet with fuselage mounted engines. The lateral attenuation adjustment in INM7.0 is slightly larger than INM6.2a for jet with fuselage mounted engines, which might cause the slight shrink of LAMAX noise contours in those three airports.

4.2 Terrain Contour Area Data (C2 &C3)

Table 7. Terrain Contour Area Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY with Terrain	C2	6.2a/7.0	On	No Prop Attenuation	Off	59°F	8 Knots
STUDY with and without Terrain, 7.0 Release Only	C3	7.0 only	On/Off	No Prop Attenuation	Off	59°F	8 Knots

	DNL	%	Area Change II	LAMAX	% /	Ar		
	LEVEL	Western	Eastern	LgHub	LgGA	LEVEL	Western	Г
	55	4.36	3.89	2.49	8.17	90	(0.94)	
	60	4.77	5.20	2.29	7.95	95	(2.27)	
ſ	65	4.31	5.10	2.64	7.99	100	(3.66)	Г
	70	2.14	3.39	0.89	8.73	105	(1.75)	

LAMAX	% /	Area Change II	NM7.0 vs INM6	5.2a
LEVEL	Western	Eastern	LgHub	LgGA
90	(0.94)	0.43	(2.09)	(1.77)
95	(2.27)	0.50	(3.36)	(0.85)
100	(3.66)	1.01	(1.99)	(3.03)
105	(1.75)	2.63	(4.94)	(1.23)

DNL	% Area Change (7.0 w/out Terrain - 7.0 with)					
LEVEL	Western	Eastern	LgHub	LgGA		
55	1.09	1.87	3.31	4.25		
60	1.38	2.98	3.41	4.21		
65	(0.73)	2.54	2.76	5.12		
70	0.17	1.68	2.82	11.46		

LAMAX	% Area Change (7.0 w/out Terrain - 7.0 with)					
LEVEL	Western	Eastern	LgHub	LgGA		
90	(7.14)	1.66	7.38	0.38		
95	(4.56)	2.23	9.01	0.72		
100	(4.26)	3.03	2.69	1.33		
105	(2.66)	1.22	1.97	0.43		

Observations and Discussion:

As shown in Table 7, the 65 dB DNL contour increases in version 7.0 with Terrain on, but to a lesser extent than seen in the baseline. This is due to the Line-of-Sight blockage that the Terrain "On" invokes, which, if large enough, could supersede the lateral attenuation adjustment for certain operations. This is because the lateral attenuation adjustment is compared to the line-of-site blockage adjustment, and only the larger of the two is implemented, which results in a non-linear combination of these effects.

The change seen between turning on and off terrain processing in version 7.0 is as expected.

4.3 Lateral Attenuation Contours (C4 & C5)

Table 8. Lateral Attenuation Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY with Lateral Attenuation On (All Soft Ground)	C4	6.2a/7.0	Off	All Soft Ground	Off	59°F	8 Knots
STUDY with and without Lateral Attenuation, 7.0 Release Only	C5	7.0 only	Off	All Soft Ground / No- Prop- Attenuation	Off	59°F	8 Knots

DNL	% Area Change INM7.0 vs INM6.2a					
LEVEL	Western	Western Eastern LgHub				
55	6.54	5.94	3.62	11.97		
60	6.92	8.39	3.36	10.35		
65	6.28	7.61	3.89	10.13		
70	3.76	4.37	1.63	11.42		

LAMAX	% Area Change INM7.0 vs INM6.2a					
LEVEL	Western	Eastern	LgHub	LgGA		
90	(0.04)	2.24	(0.77)	(1.55)		
95	(3.58)	2.93	(2.89)	(0.72)		
100	(3.64)	4.14	(3.01)	(2.83)		
105	(4.45)	3.78	(5.33)	(1.68)		

DNL	% Area Change (7.0 without LatAtten - 7.0 with)				
LEVEL	Western	Eastern	LgHub	LgGA	
55	0.37	0.39	0.86	7.30	
60	0.45	0.65	0.80	7.83	
65	0.62	1.16	1.04	8.47	
70	0.59	0.73	0.56	16.07	

LAMAX	% Area Change (7.0 without LatAtten - 7.0 with)					
LEVEL	Western	Eastern	LgHub	LgGA		
90	-	-	-	0.23		
95	-	-	-	0.29		
100	-	-	-	0.36		
105	-	-	-	0.16		

Observations and Discussion:

Table 8 show that the DNL contour increased in version 7.0 by a larger amount than in the baseline setting (Section 3.1) for the "All Soft Ground" conditions, where lateral attenuation was applied to all aircraft in the study (see Figure 2 for lateral attenuation effects).

In general, the new lateral attenuation implementation can result in up to a 3 dB difference between versions 6.2a and 7.0 for propeller aircraft and helicopters, up to a 2.5 dB difference for aircraft with wing-mounted engines, and up to 1 dB difference for aircraft with fuselage-mounted engines. These differences are dependant on slant range distance and elevation angle, as well as aircraft type. The differences in lateral attenuation adjustment (especially the decrease in lateral attenuation for aircraft with wing-mounted engines) are on par with the observed DNL contour area change.

The changes seen in version 7.0 with and without lateral attenuation are as expected. This variable only turned on and off lateral attenuation for propeller aircraft and helicopters in version 7.0, and the small changes in contour area in the "Eastern," "Western," and "LgHub" were attributed to the small number of propeller aircraft in the studies. The "LgGA" airport shows the large increase in DNL because props dominated the fleet at that airport.

The LAMAX contours in version 7.0 were barely affected by the turn-on/off of lateral attenuation. For jet dominated airports, there is essentially no difference, which was expected. Even for the "LgGA" airport, the changes were small indicating that jets are likely the dominant maximum noise contribution, even though they are minority of the fleet. This observation was consistent with the reasoning on the DNL contour change in the baseline setting in Section 4.1.

4.4 Bank Angle Contours (C6 & C7)

Table 9. Bank Angle Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY 6.2a Baseline vs. 7.0 Release with Bank Angle	C6	6.2a/7.0	Off	No Prop Attenuation	On	59°F	8 Knots
STUDY, 7.0 Release with and without Bank Angle	C 7	7.0 only	Off	No Prop Attenuation	On/Off	59°F	8 Knots

DNL	% Area Change INM7.0 vs INM6.2a					
LEVEL	Western	Eastern	LgHub	LgGA		
55	5.15	5.64	2.34	9.43		
60	5.23	7.40	2.69	8.86		
65	5.50	6.86	2.98	9.24		
70	3.09	3.19	1.36	10.95		

LAMAX	% Area Change INM7.0 vs INM6.2a					
LEVEL	Western	Eastern	LgHub	LgGA		
90	(0.33)	2.40	(1.03)	(2.85)		
95	(4.46)	2.93	(3.46)	(1.60)		
100	(4.56)	5.24	(2.62)	(3.50)		
105	(4.88)	4.56	(4.29)	(2.12)		

DNL	% Area Change (7.0 without Bank Angle - 7.0 with)					
LEVEL	Western Eastern		LgHub	LgGA		
55	0.48	0.07	0.96	1.22		
60	0.78	0.65	0.37	0.48		
65	0.23	0.29	0.17	0.10		
70	0.11	0.90	0.02	0.07		

LAMAX	% Area Change (7.0 without Bank Angle - 7.0 with)					
LEVEL	Western Eastern		LgHub	LgGA		
90	0.14	(0.15)	0.15	1.25		
95	1.06	0.00	0.59	0.80		
100	0.96	(1.05)	(0.40)	0.63		
105	0.46	(0.74)	(1.09)	0.46		

Observations and Discussion:

It is important to note that because the bank angle functionality was not available prior to the release of version 7.0, it could not be fully exercised in the version 6.2a and 7.0 comparisons. Therefore the focus of this analysis was on the contour change in version 7.0 with and without bank angle.

Since bank angle primarily impacts lateral attenuation, the focus of this analysis was the less than 1% change in the area of the 65 dB DNL contour in version 7.0 with and without bank angle. This change is largely due to the effects of engine installation effects for jets, though aircraft performance does play a small role. In general, bank angle affects the directionality of noise contours (minimally affecting contour shape) but only has a minor impact on overall contour area, as seen in Table 9.

4.5 **Different Temperature Contours (C8 – C11)**

Table 10. Different Temperature Results

	1	abic 10. Dii	ici chi i chi	perature resu	113		
Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY at 100° F	C8	6.2a/7.0	Off	No Prop	Off	100°F	8 Knots
310D1 at 100 1	Co	0.24/1.0	OII	Attenuation	OII	1001	O KIIOIS
7.0 Release at 59° F	C9	7.0 only	Off	No Prop	Off	100°F/59°F	8 Knots
and 100° F	C-9	7.0 Ully	OII	Attenuation	OII	100 1755 1	O KIIOIS
STUDY at 32° F	C10	6.2a/7.0	Off	No Prop	Off	32°F	8 Knots
31001 at 32 1	CIU	0.24/1.0	OII	Attenuation	OII	321	o Kilots
7.0 Release at 59° F	C11	7.0 only	Off	No Prop	Off	32°F/59°F	8 Knots
and 32° F	CII	7.0 Ully	OII	Attenuation	OII	32 1/35 1	O KIIUIS

Table 10. Different Temperature Results (continued)

% Area Change INM7.0 vs INM6.2a									
Western		Eastern		LgHub		LgGA			
32"	100°	32°	100°	32°	100°	32'	100°		
5.20	5.78	5.64	5.78	3.18	3.33	10.71	10.86		
6.15	8.38	7.66	8.38	3.05	2.85	9.64	9.51		
5.88	6.89	7.48	6.89	3.13	3.11	9.46	8.91		
4.29	3.18	4.61	3.18	1.64	1.16	10.17	12.14		
	32° 5.20 6.15 5.88	32' 100' 5.20 5.78 6.15 8.38 5.88 6.89	Western Eas 32° 100° 32° 5.20 5.78 5.64 6.15 8.38 7.66 5.88 6.89 7.48	Western Eastern 32' 100' 32' 100' 5.20 5.78 5.64 5.78 6.15 8.38 7.66 8.38 5.88 6.89 7.48 6.89	Western Eastern Lgt 32° 100° 32° 100° 32° 5.20 5.78 5.64 5.78 3.18 6.15 8.38 7.66 8.38 3.05 5.88 6.89 7.48 6.89 3.13	Western Eastern LgHub 32° 100° 32° 100° 32° 100° 5.20 5.78 5.64 5.78 3.18 3.33 6.15 8.38 7.66 8.38 3.05 2.85 5.88 6.89 7.48 6.89 3.13 3.11	Western Eastern LgHub Lg 32' 100' 32' 100' 32' 5.20 5.78 5.64 5.78 3.18 3.33 10.71 6.15 8.38 7.66 8.38 3.05 2.85 9.64 5.88 6.89 7.48 6.89 3.13 3.11 9.46		

LAMAX			% Area	Change II	M7.0 vs IN	M6.2a		
LEVEL	/EL Western		Eastern		LgHub		LgGA	
	32"	100°	32°	100°	32°	100°	32'	100°
90	(0.58)	(0.13)	2.75	2.43	(0.63)	(1.03)	(1.39)	(1.26)
95	(3.51)	(3.32)	3.52	3.55	(2.56)	(3.00)	(1.34)	(1.18)
100	(4.45)	(3.79)	3.13	3.62	(3.95)	(4.50)	(3.65)	(2.12)
105	(7.71)	(4.36)	0.50	3.91	(4.15)	(8.34)	(1.90)	(2.22)
105	(7.71)	(4.36)	0.50	3.91	(4.15)	(8.34)	(1.90)	(2.

DNL		% Area Change INM7.0 at stated Temp vs INM7.0 at 59°									
LEVEL	Wes	stern	Eastern		LgHub		LgGA				
	32"	100°	32"	100°	32"	100°	32°	100°			
55	4.41	(6.92)	4.04	(4.45)	8.91	(11.51)	5.03	(8.05)			
60	5.47	(9.02)	5.10	(7.70)	7.87	(9.96)	3.25	(7.46)			
65	4.30	(8.11)	3.44	(4.17)	7.94	(10.74)	3.08	(9.62)			
70	5.05	(11.35)	1.10	(3.71)	6.15	(8.20)	2.99	(14.52)			

I	LAMAX		% Are	a Change I	NM7.0 at s	tated Temp	vs INM7.0	at 59°	
	LEVEL	Wes	stern	n Eastern		Lgl	lub	LgGA	
		32"	100°	32"	100°	32"	100°	32"	100°
	90	(1.10)	9.25	0.49	0.85	(2.86)	(1.97)	(3.58)	(1.60)
	95	(1.77)	1.57	0.69	(1.12)	(2.13)	4.19	(3.61)	8.83
[100	(3.94)	16.77	(0.99)	7.32	(2.96)	22.18	(4.65)	(20.46)
	105	(12.68)	34.22	(3.24)	9.28	(5.37)	37.07	(3.83)	2.49

Observations and Discussion:

The way temperature is handled in INM does not change between version 6.2a and version 7.0. This comparison provides an understanding of how temperature change can affect a study.

Airport temperature affects aircraft performance and noise adjustments (atmospheric absorption and acoustic impedance). Since the temperature-affected noise adjustments were unchanged between version 6.2a and 7.0, the changes observed in this study were related to the indirect effect of temperature on aircraft performance. The area change in the 65 dB DNL contours between version 6.2a and version 7.0 in Table 10 was expected. With the improvements in the modeling methodologies, the contours increased in INM 7.0 regardless of the temperature.

When comparing version 7.0 at the different temperatures, the expected changes in the DNL contours are seen. A higher temperature results in a decrease in thrust which causes a reduction in the climb rate, which may decrease DNL, while a lower temperature causes the opposite effect on thrust and climb rate. This behavior is consistent with previous versions on INM.

4.6 Different Headwind Contours (C12 -- C15)

Table 11. Different Headwind Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY with -8 Knot Headwind	C12	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	-8 Knots
7.0 Release with +8 Knot and -8 Knot Headwind	C13	7.0 only	Off	No Prop Attenuation	Off	59°F	-8/+8 Knots
STUDY with Zero Headwind	C14	6.2a/7.0	Off	No Prop Attenuation	Off	59°F	0 Knots
7.0 Release with 8Kt and Zero Headwind	C15	7.0 only	Off	No Prop Attenuation	Off	59°F	8 / 0 Knots

Table 11. Different Headwind Results (continued)

	% Area Change INM7.0 vs INM6.2a									
Wes	Western		Eastern		LgHub		LgGA			
-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots			
0.25	2.59	1.23	3.55	(0.88)	1.19	1.18	5.56			
(0.58)	2.57	0.99	4.52	(1.13)	0.86	2.44	5.85			
(1.46)	1.62	(0.06)	3.47	(2.03)	0.57	2.76	5.82			
(4.03)	(0.02)	(1.80)	1.36	(3.41)	(1.09)	1.31	5.02			
	-8 Knots 0.25 (0.58) (1.46)	-8 Knots 0 Knots 0.25 2.59 (0.58) 2.57 (1.46) 1.62	Western Eas -8 Knots 0 Knots -8 Knots 0.25 2.59 1.23 (0.58) 2.57 0.99 (1.46) 1.62 (0.06)	Western Eastern -8 Knots 0 Knots -8 Knots 0 Knots 0.25 2.59 1.23 3.55 (0.58) 2.57 0.99 4.52 (1.46) 1.62 (0.06) 3.47	Western Eastern Lgt -8 Knots 0 Knots -8 Knots 0 Knots -8 Knots 0.25 2.59 1.23 3.55 (0.88) (0.58) 2.57 0.99 4.52 (1.13) (1.46) 1.62 (0.06) 3.47 (2.03)	Western Eastern LgHub -8 Knots 0 Knots -8 Knots 0 Knots -8 Knots 0 Knots 0.25 2.59 1.23 3.55 (0.80) 1.19 (0.58) 2.57 0.99 4.52 (1.13) 0.86 (1.46) 1.62 (0.06) 3.47 (2.03) 0.57	Western Eastern LgHub Lg -8 Knots 0 Knots -8 Knots 0 Knots -8 Knots 0 Knots -8 Knots 0.25 2.59 1.23 3.55 (0.88) 1.19 1.18 (0.58) 2.57 0.99 4.52 (1.13) 0.86 2.44 (1.46) 1.62 (0.06) 3.47 (2.03) 0.57 2.76			

LAMAX % Area Change INM7.0 vs INM6.2a									
LEVEL	Wes	tern	Eas	tern	Lg⊦	LgHub		LgGA	
	-8 Knots	0 Knots							
90	(0.22)	(0.09)	2.28	2.31	(0.83)	(0.76)	(1.18)	(0.92)	
95	(3.26)	(3.37)	2.87	2.94	(2.60)	(3.16)	(0.44)	(0.15)	
100	(3.33)	(3.84)	3.32	3.53	(3.10)	(3.34)	(2.08)	(2.97)	
105	(7.90)	(5.08)	3.40	3.99	(5.48)	(4.18)	(1.95)	(2.05)	

	DNL	% A	rea Chang	e INM7.0 at	% Area Change INM7.0 at stated Headwind vs INM7.0 at a 8 KT Headwind								
	LEVEL	Wes	stern	Eastern		LgHub		LgGA					
		-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots				
	55	2.07	1.15	2.55	1.27	2.96	1.46	3.07	1.38				
	60	1.78	0.84	0.83	0.43	3.36	1.59	3.75	1.72				
	65	3.47	1.45	5.89	2.71	4.33	2.53	3.04	1.37				
Ī	70	2.14	1.61	6.40	3.01	6.65	3.18	3.73	1.90				

٦	LAMAX	% A	rea Chang	e INM7.0 at	stated Hea	adwind vs IN	M7.0 at a	8 KT Heady	vind
	LEVEL	Wes	stern	Eastern Lg		Lgl	lub	LgGA	
		-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots	-8 Knots	0 Knots
1	90	18.93	8.38	8.46	4.13	22.82	10.51	24.27	12.00
	95	28.30	14.14	7.54	4.00	29.80	13.87	28.99	15.10
	100	39.14	19.38	11.86	5.38	37.03	17.91	34.87	16.61
1	105	77.74	31.30	12.07	5.90	41.53	18.37	36.87	15.54

Observations and Discussion:

The methodology of how headwind is handled in INM does not change between version 6.2a and version 7.0. A coding error with the aircraft ground speed reporting was discovered in version 6.2a and subsequently corrected in version 7.0. This comparison provides an understanding of how headwind change can affect a study and verifies the coding error fix.

The results presented in Table 11 verify that the fix has been properly implemented in INM 7.0. In addition, the use of the -8 or 0 KT headwinds in version 7.0 causes an increase in contour size for both DNL and LAMAX compared to an 8 KT headwind. This increase is caused by the performance effects associated with reduced headwind; such as reduced climb angles and increased acceleration distances relative to the ground.

Note: the increase in LAMAX contours at the Eastern airport for version 7.0 when compared to version 6.2a is the result of the Lateral Attenuation adjustment described in Section 4.3.

4.7 All Variables On Contours (C16 & C17)

Table 12. All "Variables On" Results

Study Name	Case #	INM versions	Terrain	Lateral Attenuation	Bank Angle	Temperature	Headwind
STUDY All Variables On	C16	6.2a/7.0	On	All Soft Ground	On	59°F	8 Knots
Baseline vs. All Variables On, 7.0 Release	C17	7.0 only	On/Off	All Soft Ground / No- Prop- Attenuation	On/Off	59°F	8 Knots

DNL	%	% Area Change INM7.0 vs INM6.2a								
LEVEL	Western	Eastern	LgHub	LgGA						
55	4.29	4.09	1.93	9.14						
60	4.25	4.96	2.08	8.75						
65	4.25	5.33	2.86	9.06						
70	2.16	3.01	0.99	9.80						

LAMAX	% Area Change INM7.0 vs INM6.2a				
LEVEL	Western	Eastern	LgHub	LgGA	
90	(1.06)	0.59	(2.20)	(2.90)	
95	(3.26)	0.55	(3.98)	(1.63)	
100	(4.60)	1.81	(1.94)	(3.63)	
105	(2.27)	3.28	(2.46)	(1.88)	

DNL	% Area Change (7.0 Baseline - 7.0 All Variables On)				
LEVEL	Western	Eastern	LgHub	LgGA	
55	1.56	2.08	4.73	10.09	
60	2.33	3.79	4.40	9.42	
65	(0.28)	3.38	3.76	9.62	
70	0.50	2.80	3.24	18.22	

LAMAX	% Area Change (7.0 Baseline - 7.0 All Variables On)				
LEVEL	Western	Eastern	LgHub	LgGA	
90	(7.03)	1.50	7.57	1.68	
95	(3.59)	2.18	9.71	1.58	
100	(3.32)	2.22	2.63	2.01	
105	(2.14)	0.60	(0.63)	1.09	

Observations and Discussion:

Table 12 shows the DNL contour increase between versions 6.2a and 7.0 for the "All Variables On" conditions, similar to the increases seen in the terrain condition comparison in Section 4.1. Figure 4 shows this comparison for the "LgGA" airport study. As illustrated in the figure, though the percent increase in the 70 dB DNL contour is large for the "LgGA" airport, the overall area of the 70 dB DNL contour in both versions is quite. It is also important to note that the percent contour area changes between versions 6.2a and 7.0 for the 65 dB DNL contour for the "All Variables On" conditions were within 10% of those changes shown for the "Baseline" conditions in Table 6, showing similar data trends.

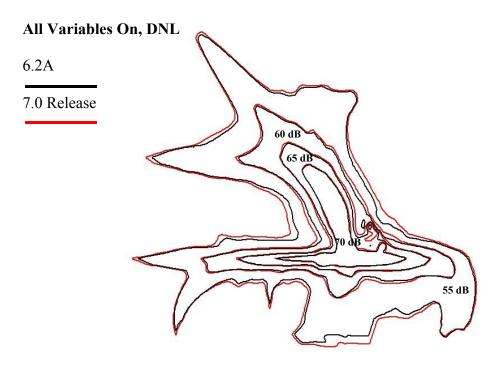


Figure 4. All Variables On (C16) DNL Contour of Airport "LgGA"

Figure 5 shows the DNL contour increase between the "Baseline" and "All Variables On" conditions for INM 7.0. These differences were on par with those seen for Lateral Attenuation in Table 8 (see Section 4.3), which implies lateral attenuation updates in version 7.0 is the dominate factor in the increase of DNL contours.

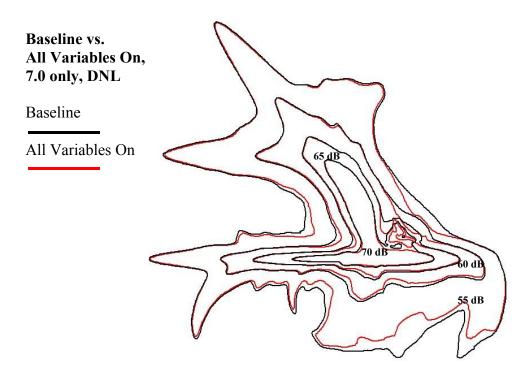


Figure 5. Baseline vs. All Variables On (C17) DNL Contour of Airport "LgGA", INM 7.0 only

It is important to note that terrain, lateral attenuation, and bank angle are not mutually exclusive. The effects of just one variable cannot be distinguished from the other two. For example, though propeller aircraft and helicopters are affected by lateral attenuation, the lateral attenuation of propeller aircraft and helicopters not affected by bank angle. Also, once terrain is turned on, the lateral attenuation adjustment is compared to the line-of-sight blockage adjustment, which results in a non-linear combination of the two effects.

5. Conclusions & Recommendations

Overall, this analysis showed that version 7.0 increases DNL noise levels as expected, but the area change generally did not exceed 10% for the four airports studied³.

Multiple updates in version 7.0 contributed to this change, but it was evident that the change in lateral attenuation was the main contributing factor to the differences seen between versions 6.2a and 7.0⁴. The effects of lateral attenuation were the most significant for small elevation angles and were aircraft type dependant.

Because the changes in the lateral attenuation adjustment implementation between versions 6.2a and 7.0 were largest for jets with wing-mounted engines and propeller aircraft, the percentage of jets with wing-mounted engines in the total fleet can be used as

⁴ This variable cannot be tested independent of other variables in INM 7.0 release version (except for prop and helicopter lateral attenuation)

³ While LAMAX contours were also analyzed, they are dominated by single aircraft events. Therefore, they do not necessarily follow the same change trend as the DNL noise contours, which are representative cumulative events at an airport.

an indicator of the DNL noise contour change, particularly when the wing-mounted jets contribute significantly to the overall noise⁵.

Parameters outside of algorithmic changes and updates (such as headwind, temperature and terrain) resulted in contour area changes in version 7.0 that were consistent with those observed in version 6.2a, as expected.

This analysis:

- (a) Was limited to multiple event studies for the DNL and LAMAX metrics;
- (b) Showed that both DNL and LAMAX noise contours changed significantly from one airport to another; and
- (c) May not represent the noise changes in single event studies;

The trends observed in the four airports studies provide a general sense of noise contour changes in using version 7.0. Good engineering judgment should be used when applying these results to other individual airports, as they may exhibit different trends from the studies in this report.

More studies are being planned to examine the effects of version 7.0 on single events, including helicopters.

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This indicator was applied to a separate airport study conducted by AEE which has wing-mounted jet accounting for 52% of the fleet. The DNL65 contour area increase is in the range of 1-2% in INM7.0 - consistent with observation in this study.